

# VGS A4



## FULL THREAD CONNECTOR WITH COUNTERSUNK HEAD

### A4 | AISI316

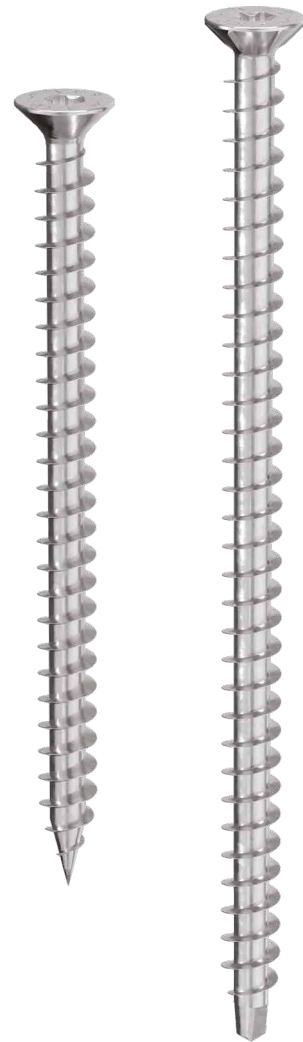
A4 | AISI316 austenitic stainless steel for high corrosion resistance. Ideal for environments adjacent to the sea in corrosivity class C5 and for insertion on the most aggressive timbers in class T5.

### T5 TIMBER CORROSIVITY

Suitable for use in applications on aggressive woods with an acidity (pH) level below 4 such as oak, Douglas fir and chestnut, and in wood moisture conditions above 20%.

### EXPOSED STRUCTURAL USE

VGS A4 is the structural wood screw with total thread, perfect for making joints that require high tension or sliding strength in extremely aggressive environments.



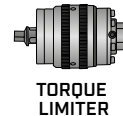
MANUALS



BIT INCLUDED

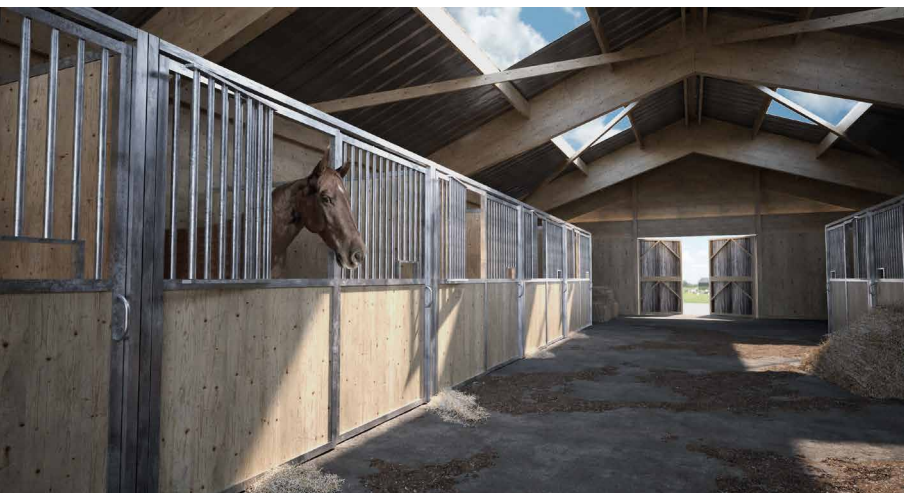
DIAMETER [mm]	9 (9) 11) 15
LENGTH [mm]	80 (100 600) 2000
SERVICE CLASS	SC1 SC2 SC3 SC4
ATMOSPHERIC CORROSIVITY	C1 C2 C3 C4 C5
WOOD CORROSIVITY	T1 T2 T3 T4 T5
MATERIAL	<b>A4</b> AISI 316 A4   AISI316 austenitic stainless steel (CRC III)

METAL-to-TIMBER recommended use:



### FIELDS OF USE

- timber based panels
- solid timber and glulam
- CLT and LVL
- ACQ, CCA treated timber



## HYBRID STEEL-TIMBER STRUCTURES

Ideal for steel structures where high-strength customised connections are required, particularly in adverse climatic contexts such as the marine environment and acidic woods.

## SWELLING OF TIMBER

Application in combination with polymeric interlayers such as XYLOFON WASHER gives the joint a certain adaptability to mitigate stresses resulting from shrinkage/swelling of the wood.

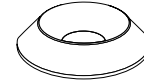


## CODES AND DIMENSIONS

A4  
AISI 316

$d_1$ [mm]	CODE	L [mm]	b [mm]	pcs
9 TX 40	VGS9120A4	120	110	25
	VGS9160A4	160	150	25
	VGS9200A4	200	190	25
	VGS9240A4	240	230	25
	VGS9280A4	280	270	25
	VGS9320A4	320	310	25
	VGS9360A4	360	350	25
11 TX 50	VGS11100A4	100	90	25
	VGS11150A4	150	140	25
	VGS11200A4	200	190	25
	VGS11250A4	250	240	25
	VGS11300A4	300	290	25
	VGS11350A4	350	340	25
	VGS11400A4	400	390	25
	VGS11500A4	500	490	25
	VGS11600A4	600	590	25

## HUS A4 - turned washer



CODE	$d_{VGS\ A4}$ [mm]	pcs
HUS8A4	9	100
HUS10A4	11	50

## RELATED PRODUCTS



### TORQUE LIMITER

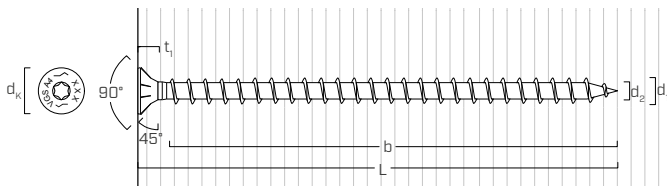
TORQUE LIMITER



### JIG VGZ 45°

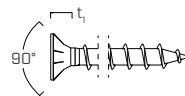
TEMPLATE FOR 45° SCREWS

## GEOMETRY AND MECHANICAL CHARACTERISTICS



### VGS Ø9

$L \leq 240$  mm

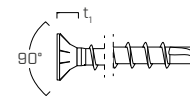


### VGS Ø11

$L \leq 250$  mm

### VGS Ø9

$240$  mm <  $L \leq 360$  mm



### VGS Ø11

$250$  mm <  $L \leq 600$  mm

Nominal diameter	$d_1$	[mm]	9	11
Head diameter	$d_k$	[mm]	16,00	19,30
Head thickness	$t_1$	[mm]	6,50	8,20
Internal thread diameter	$d_2$	[mm]	5,90	6,60
Pre-drilling hole diameter <sup>(1)</sup>	$d_{V,S}$	[mm]	5,0	6,0

<sup>(1)</sup>Pre-drilling valid for softwood.

Pre-drilling is mandatory for connectors with  $L > 400$  mm or when fastening to elements with a characteristic density  $\rho_k > 500$  kg/m<sup>3</sup>.

## CHARACTERISTIC MECHANICAL PARAMETERS

Nominal diameter	$d_1$	[mm]	9	11
Tensile strength	$f_{tens,k}$	[kN]	21,0	27,0
Yield moment	$M_{y,k}$	[Nm]	24,0	34,0
Yield strength	$f_{y,k}$	[N/mm <sup>2</sup> ]	550	550
Recommended insertion moment	$M_{ins,rec}$	[Nm]	18,0	29,0

The specified insertion moment is to be considered as the maximum applicable value; valid for applications on metal plates. Installation must stop as soon as the screw head comes into contact with the metal element.

			softwood (softwood)
Withdrawal resistance parameter	$f_{ax,k}$	[N/mm <sup>2</sup> ]	11,7
Associated density	$\rho_a$	[kg/m <sup>3</sup> ]	350
Calculation density	$\rho_k$	[kg/m <sup>3</sup> ]	$\leq 440$

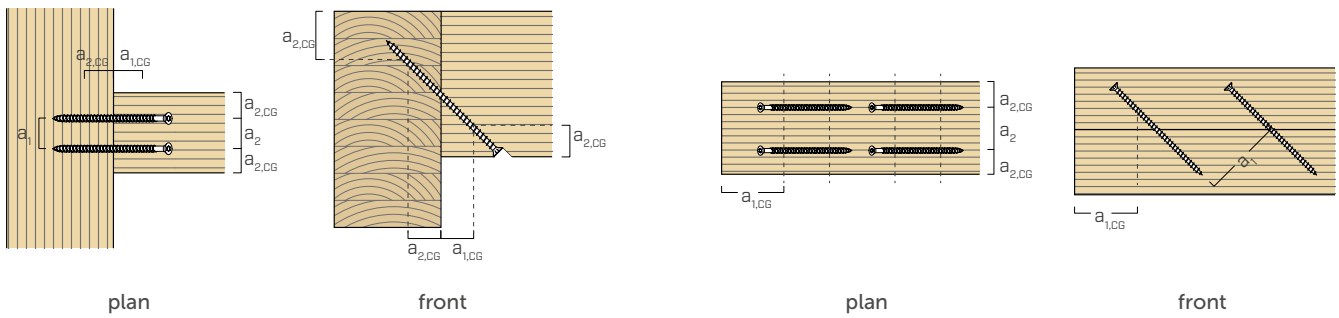
For applications with different materials please see ETA-11/0030.

## MINIMUM DISTANCES FOR AXIAL STRESSES

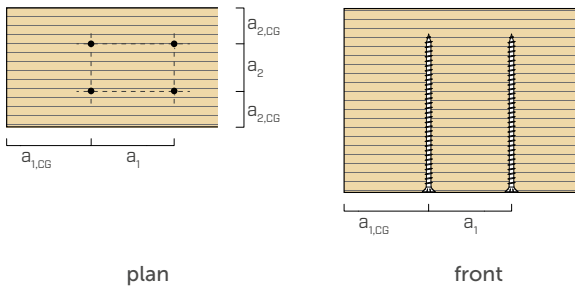
😊 screws inserted **WITH** and **WITHOUT** pre-drilled hole

$d_1$	[mm]		<b>9</b>	<b>11</b>
$a_1$	[mm]	<b>5·d</b>	45	55
$a_2$	[mm]	<b>5·d</b>	45	55
$a_{2,LIM}$	[mm]	<b>2,5·d</b>	23	28
$a_{1,CG}$	[mm]	<b>10·d</b>	90	110
$a_{2,CG}$	[mm]	<b>4·d</b>	36	44
$a_{CROSS}$	[mm]	<b>1,5·d</b>	14	17

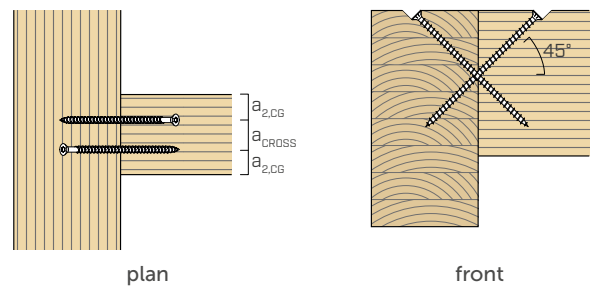
### SCREWS UNDER TENSION INSERTED WITH AN ANGLE $\alpha$ WITH RESPECT TO THE GRAIN



### SCREWS INSERTED WITH $\alpha = 90^\circ$ ANGLE WITH RESPECT TO THE GRAIN



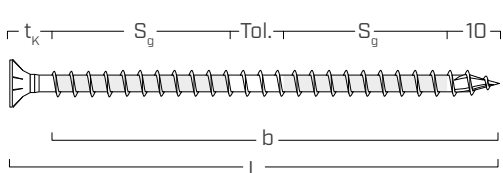
### CROSS SCREWS INSERTED WITH AN ANGLE $\alpha$ WITH RESPECT TO THE GRAIN



#### NOTES

- Minimum distances according to ETA-11/0030.
- The minimum distances are independent of the insertion angle of the connector and the angle of the force with respect to the grain.
- The axial distance  $a_2$  can be reduced down to  $a_{2,LIM}$  if for each connector a "joint surface"  $a_1 a_2 = 25 d_1^2$  is maintained.
- For minimum distances for shear load screws refer to ETA-11/0030.

## EFFECTIVE THREAD USED IN CALCULATION



$$b = S_{g,tot} = L - t_k$$

represents the entire length of the threaded part

$$S_g = (L - t_k - 10 \text{ mm} - \text{Tol.})/2$$

represents the partial length of the threaded part net of a laying tolerance (Tol.) of 10 mm

$$t_k = 10 \text{ mm (countersunk head)}$$

TENSION / COMPRESSION

geometry		total thread withdrawal				partial thread withdrawal				steel tension	instability $\epsilon=90^\circ$
		$\epsilon=90^\circ$		$\epsilon=0^\circ$		$\epsilon=90^\circ$		$\epsilon=0^\circ$			
$d_1$ [mm]	L [mm]	$S_{g,tot}$ [mm]	$A_{min}$ [mm]	$R_{ax,90,k}$ [kN]	$R_{ax,0,k}$ [kN]	$S_g$ [mm]	$A_{min}$ [mm]	$R_{ax,90,k}$ [kN]	$R_{ax,0,k}$ [kN]	$R_{tens,k}$ [kN]	$R_{ki,90,k}$ [kN]
9	120	110	130	12,50	3,75	45	65	5,11	1,53	21,00	11,54
	160	150	170	17,05	5,11	65	85	7,39	2,22		
	200	190	210	21,59	6,48	85	105	9,66	2,90		
	240	230	250	26,14	7,84	105	125	11,93	3,58		
	280	270	290	30,68	9,21	125	145	14,21	4,26		
	320	310	330	35,23	10,57	145	165	16,48	4,94		
	360	350	370	39,78	11,93	165	185	18,75	5,63		
11	100	90	110	12,50	3,75	35	55	4,86	1,46	27,00	14,57
	150	140	160	19,45	5,83	60	80	8,33	2,50		
	200	190	210	26,39	7,92	85	105	11,81	3,54		
	250	240	260	33,34	10,00	110	130	15,28	4,58		
	300	290	310	40,28	12,08	135	155	18,75	5,63		
	350	340	360	47,22	14,17	160	180	22,22	6,67		
	400	390	410	54,17	16,25	185	205	25,70	7,71		
	500	490	510	68,06	20,42	235	255	32,64	9,79		
600	590	610	81,95	24,58	285	305	39,59	11,88			

SLIDING

SHEAR

geometry		timber-to-timber				steel-to-timber				steel tension	timber-to-timber			
		$\epsilon=90^\circ$		$\epsilon=0^\circ$		$\epsilon=90^\circ$		$\epsilon=0^\circ$						
$d_1$ [mm]	L [mm]	$S_g$ [mm]	A [mm]	$B_{min}$ [mm]	$R_{V,k}$ [kN]	$S_{PLATE}$ [mm]	$S_g$ [mm]	$A_{min}$ [mm]	$R_{V,k}$ [kN]	$R_{tens,45,k}$ [kN]	$S_g$ [mm]	A [mm]	$R_{V,90,k}$ [kN]	$R_{V,0,k}$ [kN]
9	120	45	45	60	3,62	15	105	95	8,44	14,85	45	60	4,33	2,24
	160	65	60	75	5,22		145	125	11,65		65	80	4,90	2,76
	200	85	75	90	6,83		185	150	14,87		85	100	5,47	3,03
	240	105	90	105	8,44		225	180	18,08		105	120	6,04	3,20
	280	125	105	120	10,04		265	205	21,29		125	140	6,11	3,37
	320	145	120	135	11,65		305	235	24,51		145	160	6,11	3,54
	360	165	130	145	13,26		345	265	27,72		165	180	6,11	3,72
11	100	35	40	55	3,44	18	80	75	7,86	19,09	35	50	4,72	2,46
	150	60	60	75	5,89		130	110	12,77		60	75	5,98	3,16
	200	85	75	90	8,35		180	145	17,68		85	100	6,85	3,83
	250	110	95	110	10,80		230	185	22,59		110	125	7,72	4,09
	300	135	110	125	13,26		280	220	27,50		135	150	7,80	4,35
	350	160	130	145	15,71		330	255	32,41		160	175	7,80	4,61
	400	185	145	160	18,17		380	290	37,32		185	200	7,80	4,88
	500	235	180	195	23,08		480	360	47,14		235	250	7,80	5,40
600	285	215	230	27,99	580	430	56,96	285	300	7,80	5,90			

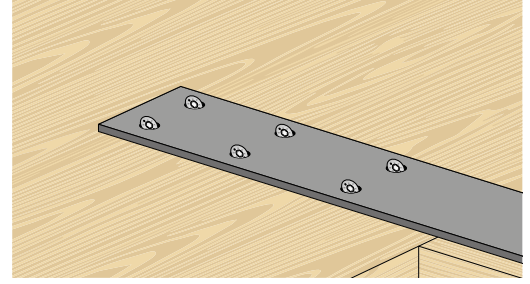
GENERAL PRINCIPLES on page 6.

## EFFECTIVE NUMBER FOR AXIAL STRESSES

The load-bearing capacity of a connection made with several screws, all of the same type and size, may be lower than the sum of the load-bearing capacities of the individual connection system.

For a connection with  $n$  screws in a metal plate application, the characteristic effective sliding load-bearing capacity is equal to:

$$R_{ef,V,k} = n_{ef,ax} \cdot R_{V,k}$$



The  $n_{ef}$  value is given in the table below as a function of  $n$  (number of screws in a row).

n	2	3	4	5	6	7	8	9	10
$n_{ef,ax}$	1,87	2,70	3,60	4,50	5,40	6,30	7,20	8,10	9,00

### STRUCTURAL VALUES

#### GENERAL PRINCIPLES

- Characteristic values comply with the EN 1995:2014 standard in accordance with ETA-11/0030.
- The tensile design strength of the connector is the lower between the timber-side design strength ( $R_{ax,d}$ ) and the steel-side design strength ( $R_{tens,d}$ ).

$$R_{ax,d} = \min \left\{ \begin{array}{l} \frac{R_{ax,k} \cdot k_{mod}}{Y_M} \\ \frac{R_{tens,k}}{Y_{M2}} \end{array} \right.$$

- The compression design strength of the connector is the lower between the timber-side design strength ( $R_{ax,d}$ ) and the instability design strength ( $R_{ki,d}$ ).

$$R_{ax,d} = \min \left\{ \begin{array}{l} \frac{R_{ax,k} \cdot k_{mod}}{Y_M} \\ \frac{R_{ki,k}}{Y_{M1}} \end{array} \right.$$

- The design sliding strength of the joint is either the timber-side design strength ( $R_{V,d}$ ) and the design strength on the steel side projected ( $R_{tens,45,d}$ ), whichever is lower:

$$R_{V,d} = \min \left\{ \begin{array}{l} \frac{R_{V,k} \cdot k_{mod}}{Y_M} \\ \frac{R_{tens,45,k}}{Y_{M2}} \end{array} \right.$$

- The design shear strength of the connector is obtained from the characteristic value as follows:

$$R_{V,d} = \frac{R_{V,k} \cdot k_{mod}}{Y_M}$$

- The coefficients  $Y_M$  and  $k_{mod}$  should be taken according to the current regulations used for the calculation.
- For the mechanical resistance values and the geometry of the screws, reference was made to ETA-11/0030.
- Sizing and verification of the timber elements and metal plates must be done separately.
- The screws must be positioned in accordance with the minimum distances.
- The characteristic thread withdrawal strengths were evaluated considering a penetration length of  $S_{g,tot}$  or  $S_g$ , as shown in the table. For intermediate values of  $S_g$  it is possible to linearly interpolate.

- The shear strength and sliding values were evaluated considering the centre of gravity of the connector placed in correspondence with the shear plane.
- The characteristic shear resistances are calculated for screws inserted without pre-drilling hole. In the case of screws inserted with pre-drilling hole, greater resistance values can be obtained.

#### NOTES

- The characteristic thread withdrawal resistances were evaluated considering both an  $\epsilon$  angle of  $90^\circ$  ( $R_{ax,90,k}$ ) and of  $0^\circ$  ( $R_{ax,0,k}$ ) between the grains of the timber element and the connector.
- The characteristic sliding strengths were evaluated by considering an angle  $\epsilon$  of  $45^\circ$  between the grains of the timber element and the connector.
- The plate thickness ( $S_{PLATE}$ ) are understood to be the minimum values to allow the head of the screw to be accommodated.
- The characteristic timber-to-timber shear strengths were evaluated considering both an  $\epsilon$  angle of  $90^\circ$  ( $R_{V,90,k}$ ) and  $0^\circ$  ( $R_{V,0,k}$ ) between the grains of the second element and the connector.
- For the calculation process a timber characteristic density  $\rho_k = 385 \text{ kg/m}^3$  has been considered.

For different  $\rho_k$  values, the strength values in the table (withdrawal, compression, sliding and shear) can be converted via the  $k_{dens}$  coefficient.

$$\begin{aligned} R'_{ax,k} &= k_{dens,ax} \cdot R_{ax,k} \\ R'_{ki,k} &= k_{dens,ki} \cdot R_{ki,k} \\ R'_{V,k} &= k_{dens,ax} \cdot R_{V,k} \\ R'_{V,90,k} &= k_{dens,V} \cdot R_{V,90,k} \\ R'_{V,0,k} &= k_{dens,V} \cdot R_{V,0,k} \end{aligned}$$

$\rho_k$ [kg/m <sup>3</sup> ]	350	380	<b>385</b>	405	425	430	440
C-GL	C24	C30	GL24h	GL26h	GL28h	GL30h	GL32h
$k_{dens,ax}$	0,92	0,98	1,00	1,04	1,08	1,09	1,11
$k_{dens,ki}$	0,97	0,99	1,00	1,00	1,01	1,02	1,02
$k_{dens,v}$	0,90	0,98	1,00	1,02	1,05	1,05	1,07

Strength values thus determined may differ, for higher safety standards, from those resulting from an exact calculation.